

μA741

FREQUENCY-COMPENSATED OPERATIONAL AMPLIFIER

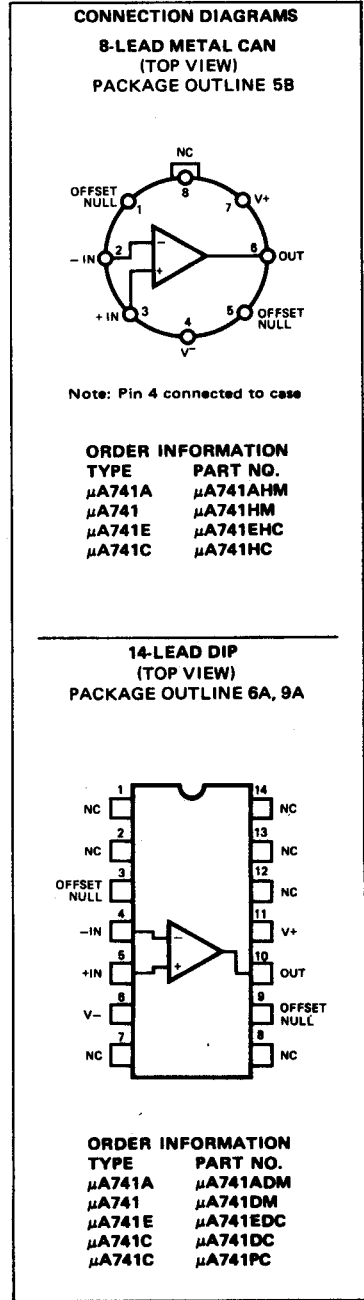
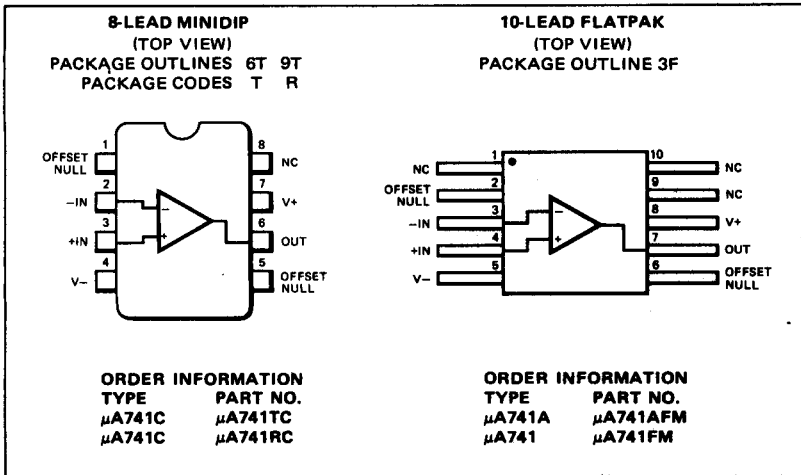
FAIRCHILD LINEAR INTEGRATED CIRCUIT

GENERAL DESCRIPTION — The μA741 is a high performance monolithic Operational Amplifier constructed using the Fairchild Planar* epitaxial process. It is intended for a wide range of analog applications. High common mode voltage range and absence of latch-up tendencies make the μA741 ideal for use as a voltage follower. The high gain and wide range of operating voltage provides superior performance in integrator, summing amplifier, and general feedback applications. Electrical characteristics of the μA741A and E are identical to MIL-M-38510/10101.

- NO FREQUENCY COMPENSATION REQUIRED
- SHORT CIRCUIT PROTECTION
- OFFSET VOLTAGE NULL CAPABILITY
- LARGE COMMON MODE AND DIFFERENTIAL VOLTAGE RANGES
- LOW POWER CONSUMPTION
- NO LATCH-UP

ABSOLUTE MAXIMUM RATINGS

Supply Voltage		±22 V
μA741A, μA741, μA741E		±18 V
μA741C		
Internal Power Dissipation (Note 1)		
Metal Can	500 mW	
Molded and Hermetic DIP	670 mW	
Mini DIP	310 mW	
Flatpak	570 mW	
Differential Input Voltage		±30 V
Input Voltage (Note 2)		±15 V
Storage Temperature Range		
Metal Can, Hermetic DIP, and Flatpak	-65°C to +150°C	
Mini DIP, Molded DIP	-55°C to +125°C	
Operating Temperature Range		
Military (μA741A, μA741)	-55°C to +125°C	
Commercial (μA741E, μA741C)	0°C to +70°C	
Lead Temperature (Soldering)		
Metal Can, Hermetic DIPs, and Flatpak (60 s)	300°C	
Molded DIPs (10 s)	280°C	
Output Short Circuit Duration (Note 3)		Indefinite



Notes on following pages.

*Planar is a patented Fairchild process.

FAIRCHILD LINEAR INTEGRATED CIRCUITS • μ A741

μ A741

ELECTRICAL CHARACTERISTICS ($V_S = \pm 15$ V, $T_A = 25^\circ$ C unless otherwise specified)

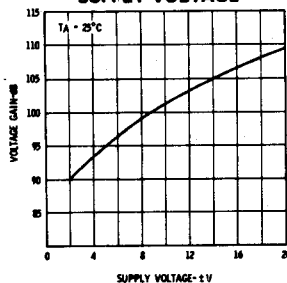
PARAMETERS (see definitions)		CONDITIONS	MIN	TYP	MAX	UNITS
Input Offset Voltage		$R_S < 10$ k Ω		1.0	5.0	mV
Input Offset Current				20	200	nA
Input Bias Current				80	500	nA
Input Resistance			0.3	2.0		M Ω
Input Capacitance				1.4		pF
Offset Voltage Adjustment Range				± 15		mV
Large Signal Voltage Gain		$R_L > 2$ k Ω , $V_{OUT} = \pm 10$ V	50,000	200,000		
Output Resistance				75		Ω
Output Short Circuit Current				25		mA
Supply Current				1.7	2.8	mA
Power Consumption				50	85	mW
Transient Response (Unity Gain)	Rise time	$V_{IN} = 20$ mV, $R_L = 2$ k Ω , $C_L < 100$ pF		0.3		μ s
	Overshoot			5.0		%
Slew Rate		$R_L > 2$ k Ω		0.5		V/ μ s

The following specifications apply for -55° C $< T_A < +125^\circ$ C:

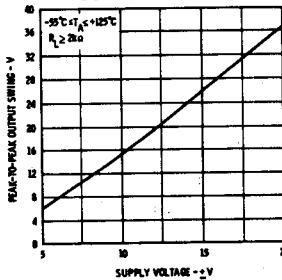
Input Offset Voltage	$R_S < 10$ k Ω		1.0	6.0	mV
Input Offset Current	$T_A = +125^\circ$ C		7.0	200	nA
	$T_A = -55^\circ$ C		85	500	nA
Input Bias Current	$T_A = +125^\circ$ C		0.03	0.5	μ A
	$T_A = -55^\circ$ C		0.3	1.5	μ A
Input Voltage Range		± 12	± 13		V
Common Mode Rejection Ratio	$R_S < 10$ k Ω	70	90		dB
Supply Voltage Rejection Ratio	$R_S < 10$ k Ω		30	150	μ V/V
Large Signal Voltage Gain	$R_L > 2$ k Ω , $V_{OUT} = \pm 10$ V	25,000			
Output Voltage Swing	$R_L > 10$ k Ω	± 12	± 14		V
	$R_L > 2$ k Ω	± 10	± 13		V
Supply Current	$T_A = +125^\circ$ C		1.5	2.5	mA
	$T_A = -55^\circ$ C		2.0	3.3	mA
	$T_A = +125^\circ$ C		45	75	mW
Power Consumption	$T_A = +125^\circ$ C		60	100	mW
	$T_A = -55^\circ$ C				

TYPICAL PERFORMANCE CURVES FOR μ A741A AND μ A741

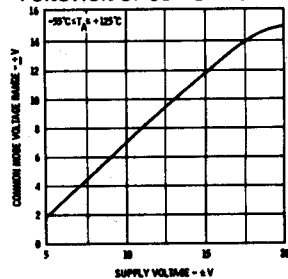
OPEN LOOP VOLTAGE GAIN AS A FUNCTION OF SUPPLY VOLTAGE



OUTPUT VOLTAGE SWING AS A FUNCTION OF SUPPLY VOLTAGE

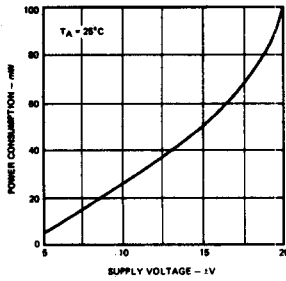


INPUT COMMON MODE VOLTAGE RANGE AS A FUNCTION OF SUPPLY VOLTAGE

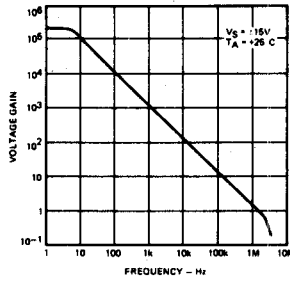


TYPICAL PERFORMANCE CURVES FOR μ A741A, μ A741, μ A741E AND μ A741C

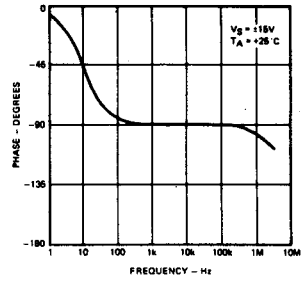
POWER CONSUMPTION AS A FUNCTION OF SUPPLY VOLTAGE



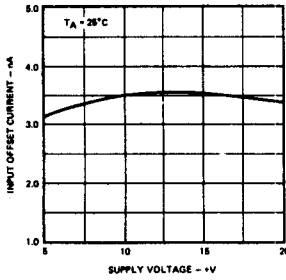
OPEN LOOP VOLTAGE GAIN AS A FUNCTION OF FREQUENCY



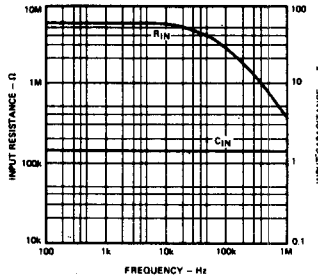
OPEN LOOP PHASE RESPONSE AS A FUNCTION OF FREQUENCY



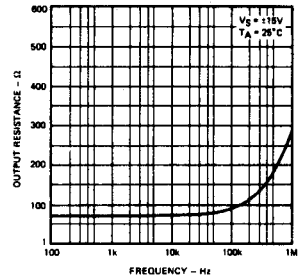
INPUT OFFSET CURRENT AS A FUNCTION OF SUPPLY VOLTAGE



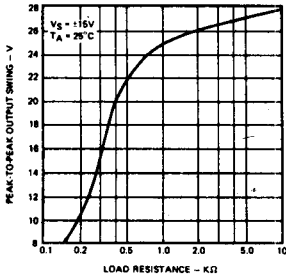
INPUT RESISTANCE AND INPUT CAPACITANCE AS A FUNCTION OF FREQUENCY



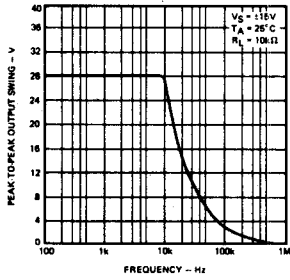
OUTPUT RESISTANCE AS A FUNCTION OF FREQUENCY



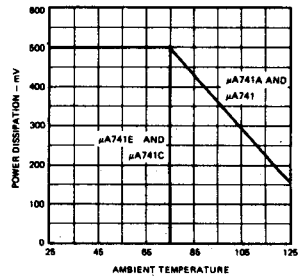
OUTPUT VOLTAGE SWING AS A FUNCTION OF LOAD RESISTANCE



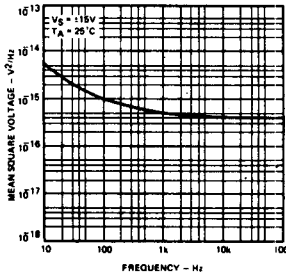
OUTPUT VOLTAGE SWING AS A FUNCTION OF FREQUENCY



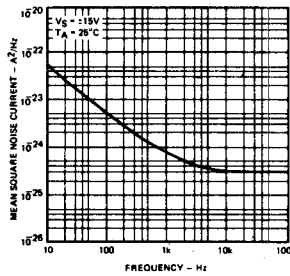
ABSOLUTE MAXIMUM POWER DISSIPATION AS A FUNCTION OF AMBIENT TEMPERATURE



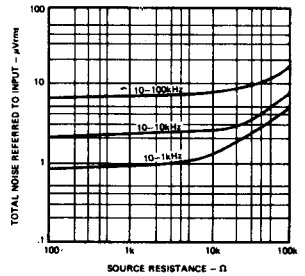
INPUT NOISE VOLTAGE AS A FUNCTION OF FREQUENCY



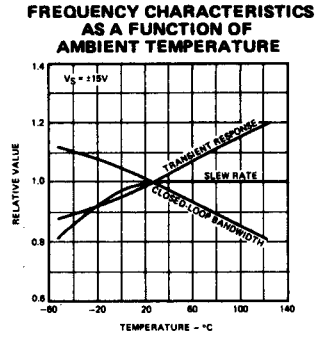
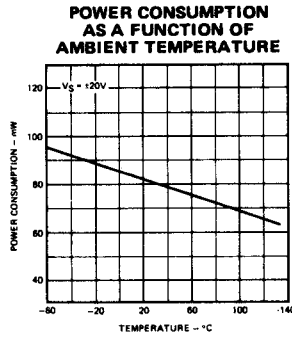
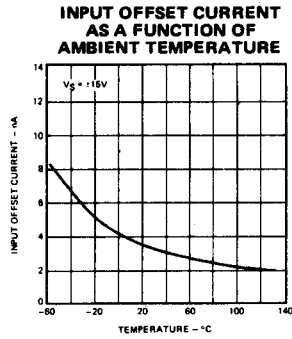
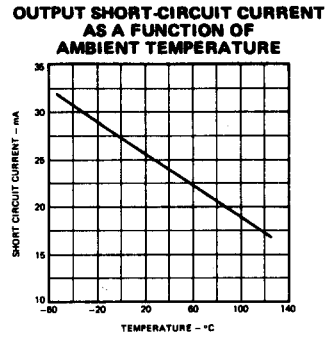
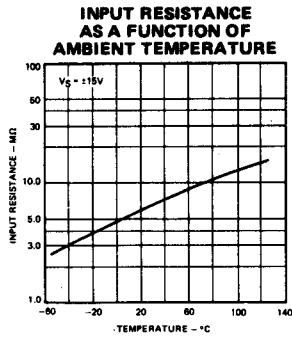
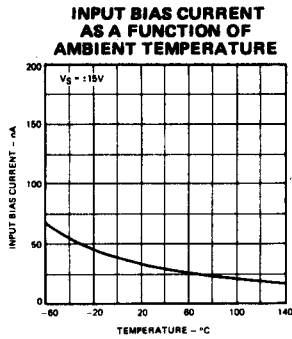
INPUT NOISE CURRENT AS A FUNCTION OF FREQUENCY



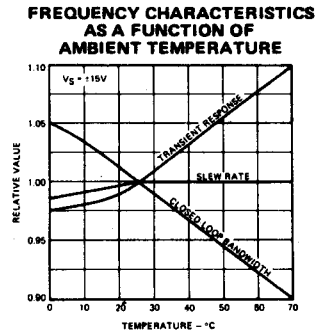
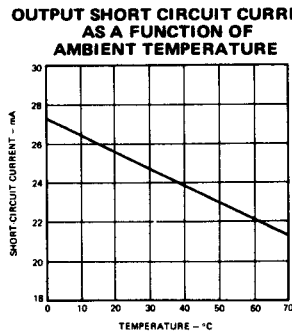
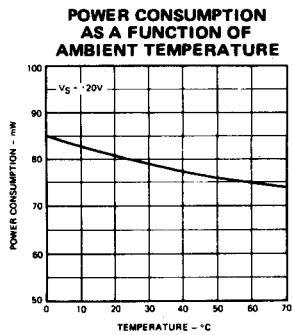
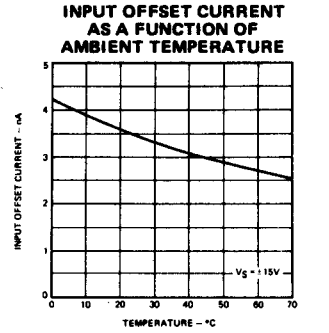
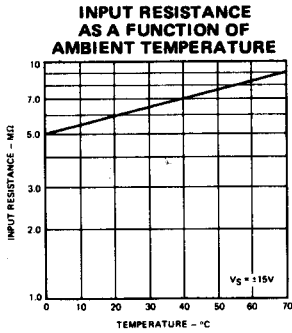
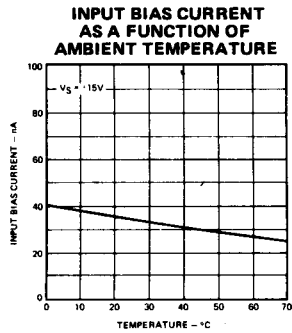
BROADBAND NOISE FOR VARIOUS BANDWIDTHS



TYPICAL PERFORMANCE CURVES FOR $\mu A741A$ AND $\mu A741$

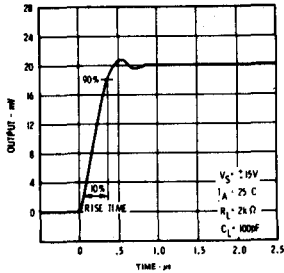


TYPICAL PERFORMANCE CURVES FOR $\mu A741E$ AND $\mu A741C$

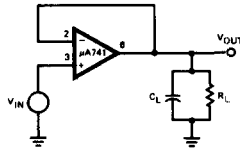


FAIRCHILD LINEAR INTEGRATED CIRCUITS • μ A741

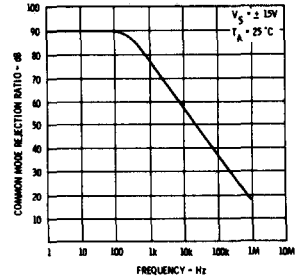
TRANSIENT RESPONSE



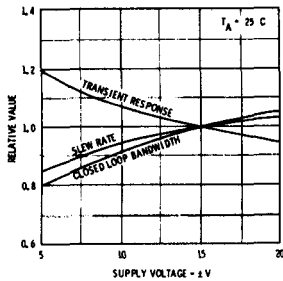
TRANSIENT RESPONSE TEST CIRCUIT



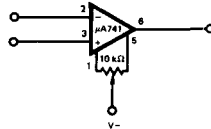
COMMON MODE REJECTION RATIO AS A FUNCTION OF FREQUENCY



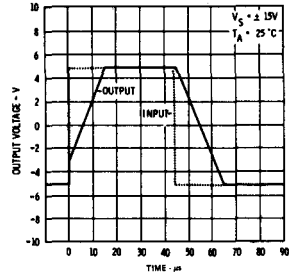
FREQUENCY CHARACTERISTICS AS A FUNCTION OF SUPPLY VOLTAGE



VOLTAGE OFFSET NULL CIRCUIT

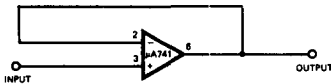


VOLTAGE FOLLOWER LARGE SIGNAL PULSE RESPONSE



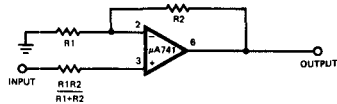
TYPICAL APPLICATIONS

UNITY-GAIN VOLTAGE FOLLOWER



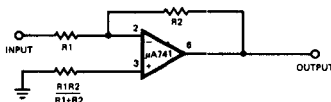
$R_{IN} = 400 \text{ M}\Omega$
 $C_{IN} = 1 \text{ pF}$
 $R_{OUT} \ll 1 \Omega$
 $B.W. = 1 \text{ MHz}$

NON-INVERTING AMPLIFIER



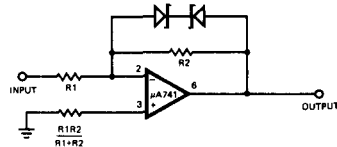
GAIN	R1	R2	BW	R_{IN}
10	1 k Ω	9 k Ω	100 kHz	400 M Ω
100	100 Ω	9.9 k Ω	10 kHz	280 M Ω
1000	100 Ω	99.9 k Ω	1 kHz	80 M Ω

INVERTING AMPLIFIER



GAIN	R1	R2	BW	R_{IN}
1	10 k Ω	10 k Ω	1 MHz	10 k Ω
10	1 k Ω	10 k Ω	100 kHz	1 k Ω
100	1 k Ω	100 k Ω	10 kHz	1 k Ω
1000	100 Ω	100 k Ω	1 kHz	100 Ω

CLIPPING AMPLIFIER

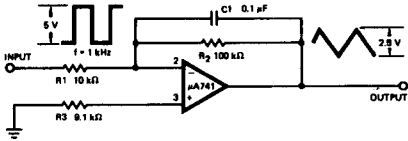


$$\frac{E_{OUT}}{E_{IN}} = \frac{R2}{R1} \text{ if } |E_{OUT}| < V_Z + 0.7 \text{ V}$$

where V_Z = Zener breakdown voltage

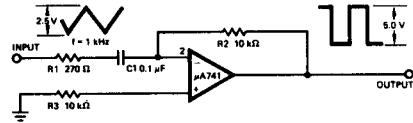
TYPICAL APPLICATIONS (Cont'd)

SIMPLE INTEGRATOR



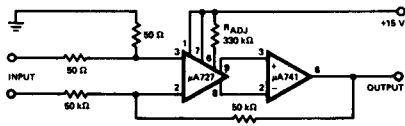
$$E_{OUT} = - \frac{1}{R_1 C_1} \int E_{IN} dt$$

SIMPLE DIFFERENTIATOR



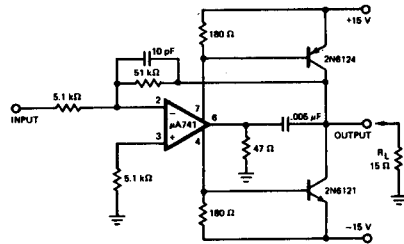
$$E_{OUT} = - R_2 C_1 \frac{dE_{IN}}{dt}$$

LOW DRIFT LOW NOISE AMPLIFIER

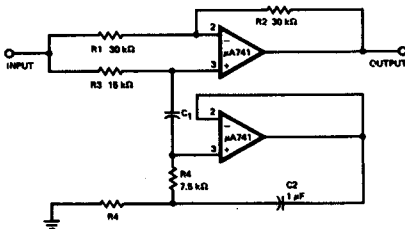


Voltage Gain = 10^3
 Input Offset Voltage Drift = $0.6 \mu V/^{\circ}C$
 Input Offset Current Drift = $2.0 pA/^{\circ}C$

HIGH SLEW RATE POWER AMPLIFIER



NOTCH FILTER USING THE μ A741 AS A GYRATOR



Trim R3 such that

$$\frac{R_1}{R_2} = \frac{R_3}{2 R_4}$$

NOTCH FREQUENCY AS A FUNCTION OF C1

